

$$\sigma = \frac{P}{A}$$

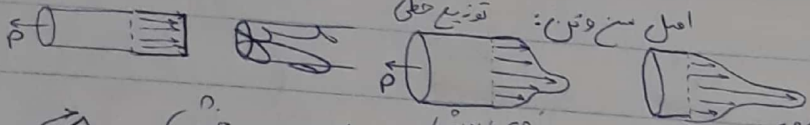
در صورت

مقاومت مصالح

الف) بار گذار محوری - توزیع تنش و انحراف

ب) بار گذار خمشی - توزیع تنش و انحراف

- (1) تنش محوری (برساز)
- (2) تنش برشی
- (3) تنش نکیله‌گانه (کششی)



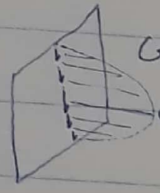
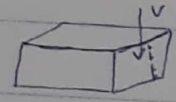
اصل مسخشون: توزیع خطی

گشتا در اول سطح $T = \frac{VQ}{I}$

گشتا در دوم سطح $T = \frac{V}{A}$

مقاومت $T = \frac{VQ}{It}$

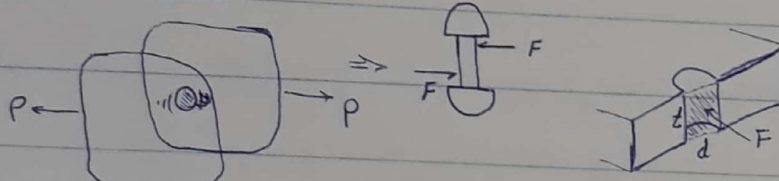
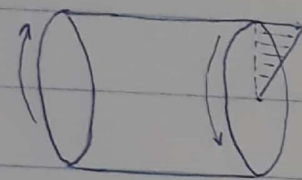
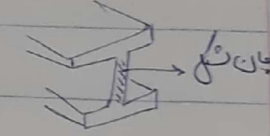
تنش برشی



ب) بار گذار پیچشی: $T = \frac{Tp}{J}$

محصول گشتا در سطح $T_{max} = \frac{3}{2} \frac{V}{A}$

محصول گشتا در سطح I شکل $T_{max} = \frac{V}{A}$



تنش نکیله‌گانه: $\sigma_b = \frac{F}{td}$

عمل $E = \frac{\sigma}{\epsilon}$

$\epsilon = \frac{\delta}{L}$

گرفتگی محوری (ع)

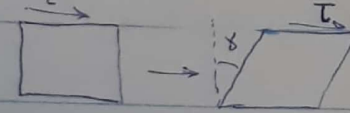
$\epsilon = \frac{\delta}{L}$

گرفتگی

$T = G\theta$

گرفتگی زاویه‌ای (ع)

عمل الاستیسیته برشی



گرفتگی جانبی - - - - -
گرفتگی طولی

گرفتگی زاویه‌ای

(نوا) فربش پواتسون

$\epsilon_x = \frac{\sigma_x}{E}$, $\epsilon_y = -\nu \frac{\sigma_x}{E}$, $\epsilon_z = -\nu \frac{\sigma_x}{E}$

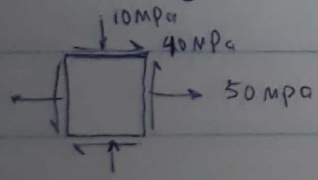
علاقه تنش و گرفتگی (تنش یک بعدی) $(\sigma_y = \sigma_z = 0)$

$\epsilon_x = \frac{\sigma_x}{E} - \nu \frac{\sigma_y}{E}$, $\epsilon_y = \frac{\sigma_y}{E} - \nu \frac{\sigma_x}{E}$, $\epsilon_z = -\nu \frac{(\sigma_x + \sigma_y)}{E}$ $(\sigma_z = 0)$

$\epsilon_x = \frac{\sigma_x}{E} - \nu \frac{(\sigma_y + \sigma_z)}{E}$, $\epsilon_y = \frac{\sigma_y}{E} - \nu \frac{(\sigma_x + \sigma_z)}{E}$

تنش سه بعدی

$\epsilon_z = \frac{\sigma_z}{E} + \nu \frac{(\sigma_x + \sigma_y)}{E}$



علاقه تنش برشی ماکزیمم

دایره مور: مثال، در حالت تنش عمودی دلخواه

الف) هر امی؟ ب) تنش بر اصلی؟

د) تنش محوری متناظر با آن؟

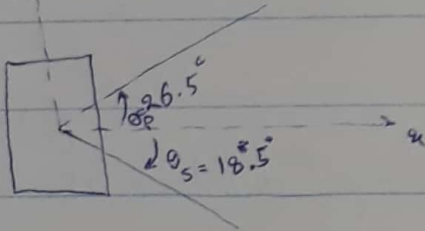
$$\sigma_x = 50 \text{ MPa}$$

$$\sigma_y = 10 \text{ MPa}$$

$$\sigma_{\text{ave}} = \frac{\sigma_x + \sigma_y}{2} = 30 \text{ MPa}$$

$$R = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2} = \sqrt{20^2 + 30^2} = 36.06 \text{ MPa}$$

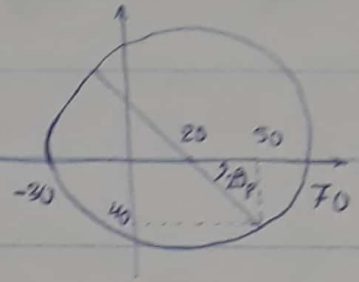
$$\tan 2\theta_p = \frac{2\tau_{xy}}{\sigma_x - \sigma_y} = \frac{60}{40} = \frac{3}{2} \rightarrow 2\theta_p = 56.3^\circ \rightarrow \theta_p = 28.15^\circ$$

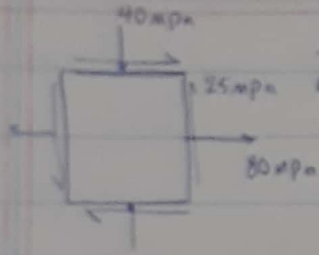


$$\tau_{\text{max}} = 36.06 \text{ MPa}$$

$$\sigma_{\text{max}} = 70 \text{ MPa}$$

$$\sigma_{\text{min}} = -30 \text{ MPa}$$





شکل حالت تنش منتهای نشان داده شده در نقطه جرفی از قطعه فولاد در مایه
 اتفاق افتاده است. بر اساس نتایج بدست آمده از پد آزمون کشش
 بهیچ نده است استخدام تسلیم برای فولاد استفاده شده $\sigma_y = 250 \text{ MPa}$
 بر باشد، مطلوب است فریب المیناخ σ_{max} استفاده
 الف) معیار ترسکا را اعمال کنید؟
 ب) معیار اعوجاج ماکسیم (فون مایس) را اعمال کنید؟

$$\sigma_{max} = \frac{80 - 40}{2} = 20 \text{ MPa}$$

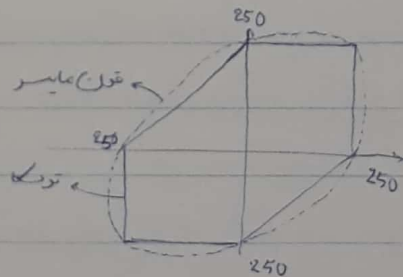
$$R = \sqrt{(80 + 40)^2 + 25^2} = 65 \text{ MPa} \rightarrow \sigma_{max} = 85 \text{ MPa} \quad \sigma_{min} = -45 \text{ MPa}$$

$$\text{معیار ترسکا: } |\sigma_1 - \sigma_3| < \sigma_y \rightarrow |85 - 45| < 250 \rightarrow 130 < 250$$

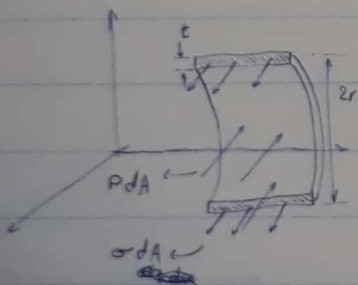
$$F_s = \frac{\sigma_y}{|\sigma_1 - \sigma_3|} = \frac{250}{130} = 1.92$$

$$\text{معیار فون مایس: } \sigma_1^2 - \sigma_1 \sigma_3 + \sigma_3^2 < \sigma_y^2 \rightarrow 85^2 - 85 \times 45 + 45^2 < 250^2 \rightarrow 13075 < 62500$$

$$F_s^2 = \frac{\sigma_y^2}{\sigma_1^2 - \sigma_1 \sigma_3 + \sigma_3^2} = \frac{62500}{13075} = 4.09 \rightarrow F_s = 2.18$$



عوارض توانایی



$$P(2r \cdot dx) - 2\sigma_1(t \cdot dx) = 0$$

$$\sigma_1 = \frac{Pr}{t}$$

تنش حلقوی

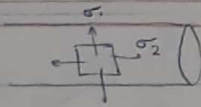


$$P(\pi r^2) = \sigma_2(2\pi r t)$$

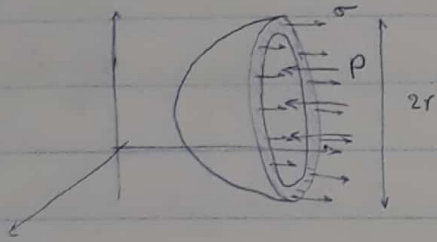
$$\sigma_2 = \frac{Pr}{2t}$$

تنش طولی

σ_x, σ_y



بر اساس معیار ترسکا:

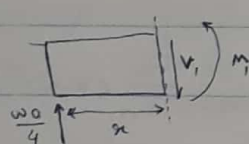
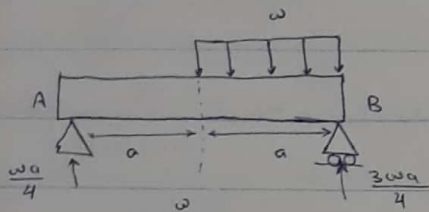


$$P(\pi r^2) - \sigma(2\pi r t) = 0$$

توزیع نیروی

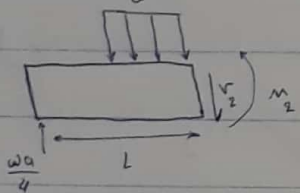
$$\sigma = \frac{Pr}{2t}$$

فصل دوم (2):



$$V_1 = \frac{wa}{4}$$

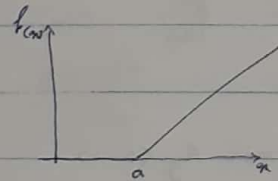
$$M_1 = \frac{wa}{4} x$$



$$V_2 = \frac{wa}{4} - w(x-a)$$

$$M_2 = \frac{wa}{4} x - \frac{w(x-a)^2}{2}$$

$$\langle x-a \rangle = \begin{cases} (x-a) & x \geq a \\ 0 & x < a \end{cases}$$



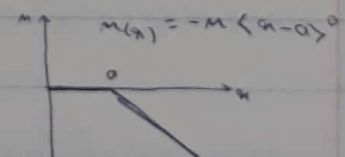
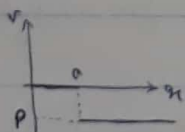
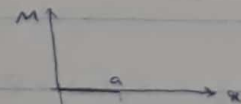
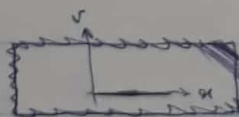
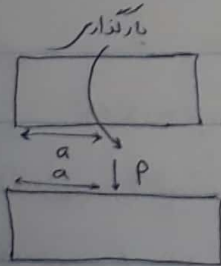
$$M(x) = \frac{wa}{4} x - \frac{w \langle x-a \rangle^2}{2}, \quad V(x) = \frac{wa}{4} - w \langle x-a \rangle$$

$$0 < x < a \rightarrow M = \frac{wa}{4} x - 0 = M_1, \quad V = \frac{wa}{4} - 0 = V_1$$

$$a < x < 2a \rightarrow M = \frac{wa}{4} x - \frac{w(x-a)^2}{2} = M_2, \quad V = \frac{wa}{4} - w(x-a) = V_2$$

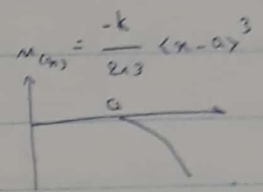
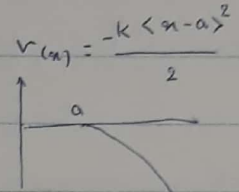
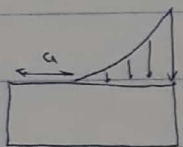
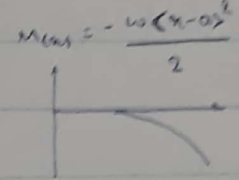
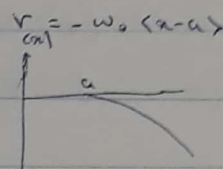
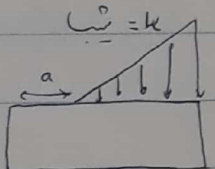
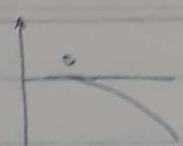
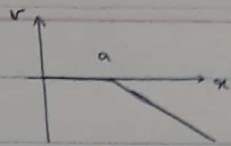
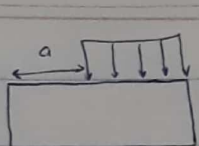
نیروی برشی

لنگه درختی



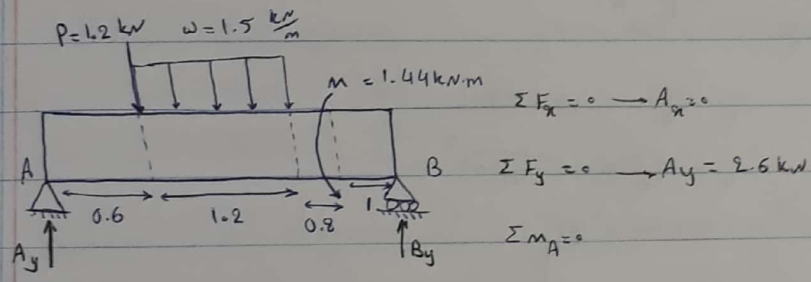
$$V(x) = -P \langle x-a \rangle^0$$

$$M(x) = -P \langle x-a \rangle^1$$



$$V_{(x)} = \frac{-k}{n+1} \langle x-a \rangle^{n+1}$$

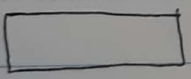
$$M_{(x)} = \frac{-k}{(n+1)(n+2)} \langle x-a \rangle^{n+2}$$



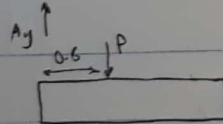
$$\sum F_x = 0 \rightarrow A_x = 0$$

$$\sum F_y = 0 \rightarrow A_y = 2.6 \text{ kN}$$

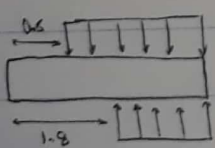
$$\sum M_A = 0$$



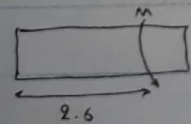
$$m_1 = A_y \langle x-0 \rangle$$



$$m_2 = -P \langle x-0.6 \rangle$$



$$m_3 = \frac{-w \langle x-0.6 \rangle^2}{2} + \frac{w \langle x-1.8 \rangle^2}{2}$$



$$m_4 = -M_0 \langle x-2.6 \rangle^0$$

$$\rightarrow m_{(x)} = A_y \langle x \rangle - P \langle x-0.6 \rangle - \frac{w \langle x-0.6 \rangle^2}{2} + \frac{w \langle x-1.8 \rangle^2}{2} - M_0 \langle x-2.6 \rangle^0$$

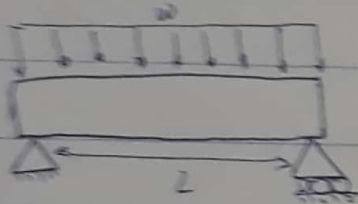
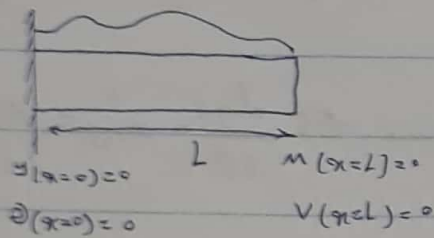
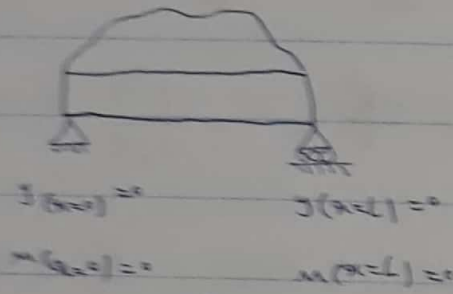
* مامثال جدول داده نمی شود، پس بجزر امت جدول را بد باسیم، در حالت کلی می توان نیورا جزو جدول نگردد و به صورت سرر حال بجزر از بللا را نوشت.

* در صورتی که مامثال مشور داسیم برای تبیح نردخ کل آن از برانتر مشور و عبات در جدول آن که مامثال $\langle x-a \rangle$ مراد است استفاد کرسیم.

$$EI \frac{d^3 y}{dx^3} = \int -w(x) dx + C_1 \quad , \quad EI \frac{d^2 y}{dx^2} = \int dx \int -w(x) dx + C_1 x + C_2$$

$$EI \frac{dy}{dx} = \int dx \int dx \int -w(x) dx + \frac{C_1}{2} x^2 + C_2 x + C_3$$

$$EI y(x) = \int dx \int dx \int dx \int -w(x) dx + \frac{C_1}{6} x^3 + \frac{C_2}{2} x^2 + C_3 x + C_4$$



$$EI \frac{d^4 y}{dx^4} = -w_0 \rightarrow EI \frac{d^4 y}{dx^4} = -w_0 \rightarrow EI \frac{d^3 y}{dx^3} = -w_0 x + C_1$$

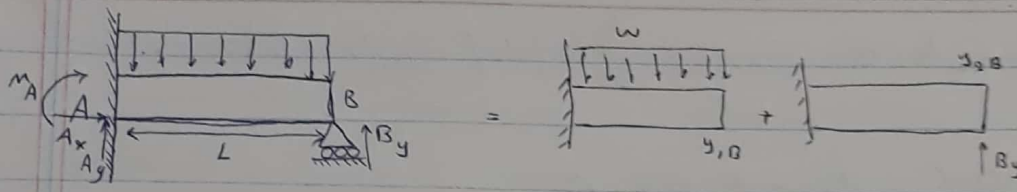
$$\rightarrow EI \frac{d^2 y}{dx^2} = -\frac{w_0}{2} x^2 + C_1 x + C_2 \rightarrow EI \frac{dy}{dx} = -\frac{w_0}{6} x^3 + \frac{C_1}{2} x^2 + C_2 x + C_3$$

$$\rightarrow EI y(x) = -\frac{w_0}{24} x^4 + \frac{C_1}{6} x^3 + \frac{C_2}{2} x^2 + C_3 x + C_4$$

$$\rightarrow y(x=0) = 0 \rightarrow C_4 = 0 \quad , \quad M(x=L) = 0 \rightarrow -\frac{w_0 L^2}{2} + C_1 L = 0 \rightarrow C_1 = \frac{w_0 L}{2}$$

$$y(x=L) = 0 \rightarrow -\frac{w_0 L^4}{24} + \frac{w_0 L}{2} \times \frac{L^3}{6} + C_3 L = 0 \rightarrow C_3 = -\frac{w_0 L^3}{24}$$

$$\rightarrow EI y(x) = -\frac{w_0 x^4}{24} + \frac{w_0 L}{2} \frac{x^3}{6} - \frac{w_0 L^3}{24} x$$



$$\begin{cases} \sum F_x = 0 \rightarrow A_x = 0 \\ \sum F_y = 0 \rightarrow A_y + B_y - w \cdot l = 0 \\ \sum M_A = 0 \rightarrow M_A + B_y \cdot l - \frac{w \cdot l^2}{2} = 0 \end{cases} \quad y_B = 0$$

$$M_{(x)} = A_y \cdot x - M_A - \frac{w \cdot x^2}{2}$$

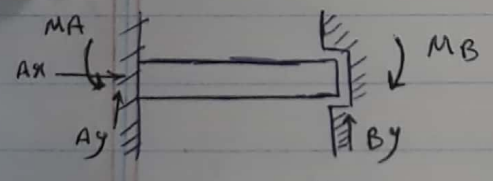
$$\frac{d^2 y}{dx^2} = \frac{M(x)}{EI} \rightarrow EI \frac{d^2 y}{dx^2} = M_{(x)} = A_y \cdot x - M_A - \frac{w \cdot x^2}{2}$$

$$EI \frac{dy}{dx} = A_y \frac{x^2}{2} - M_A \cdot x - \frac{w \cdot x^3}{6} + C_1$$

$$EI y_{(x)} = A_y \frac{x^3}{6} - M_A \frac{x^2}{2} - \frac{w \cdot x^4}{24} + C_1 \cdot x + C_2$$

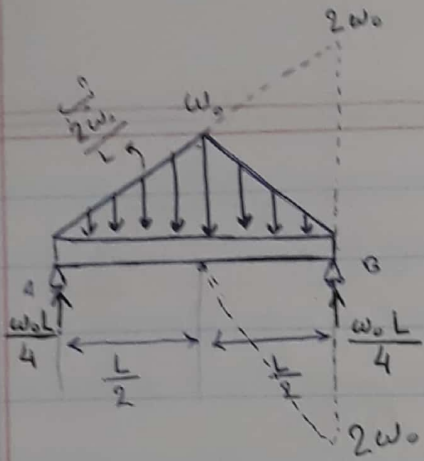
$$y_{(x=0)} = 0 \rightarrow C_2 = 0, \quad \theta_{(x=0)} = 0 \rightarrow C_1 = 0$$

$$\rightarrow EI y_{(x)} = A_y \frac{x^3}{6} - M_A \frac{x^2}{2} - \frac{w \cdot x^4}{24}$$



$$y_B = 0$$

$$\theta_B = 0$$



$$y(x) = ? , \theta_A = ?$$

$$\frac{d^2 y}{dx^2} = \frac{M(x)}{EI}$$

$$M(x) = \frac{w_0 L x}{4} - \frac{w_0}{3L} x^3 + \frac{2w_0}{3L} \left\langle x - \frac{L}{2} \right\rangle^3$$

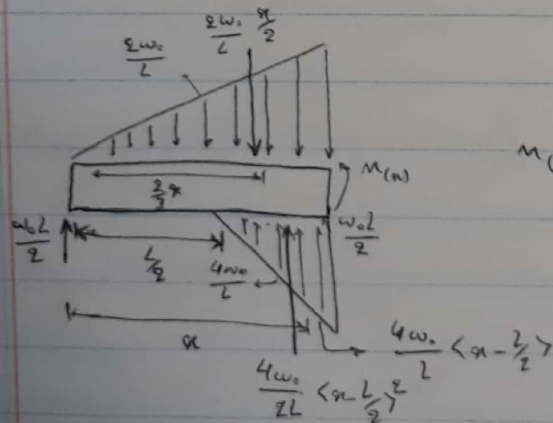
$$EI \frac{d^2 y}{dx^2} = M(x) = \frac{w_0 L}{4} x - \frac{w_0}{3L} x^3 + \frac{2w_0}{3L} \left\langle x - \frac{L}{2} \right\rangle^3$$

$$EI \frac{dy}{dx} = \frac{w_0 L}{8} x^2 - \frac{w_0}{12L} x^4 + \frac{w_0}{6L} \left\langle x - \frac{L}{2} \right\rangle^4 + C_1$$

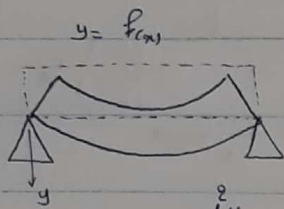
$$EI y(x) = \frac{w_0 L}{24} x^3 - \frac{w_0}{60L} x^5 + \frac{w_0}{30L} \left\langle x - \frac{L}{2} \right\rangle^5 + C_1 x + C_2$$

$$y(x=0) = 0 \rightarrow C_2 = 0, \quad y(x=L) = 0 \rightarrow C_1 = \frac{-5}{192} w_0 L^3$$

$$\rightarrow EI y(x) = \frac{w_0 L}{24} x^3 - \frac{w_0}{60L} x^5 + \frac{w_0}{30L} \left\langle x - \frac{L}{2} \right\rangle^5 - \frac{5}{192} w_0 L^3 x$$



$$M(x) = \frac{w_0 L}{4} x - \frac{2w_0 L^2}{2L} \frac{x}{3} + \frac{4w_0}{2L} \left\langle x - \frac{L}{2} \right\rangle^2 \frac{\left\langle x - \frac{L}{2} \right\rangle}{3}$$

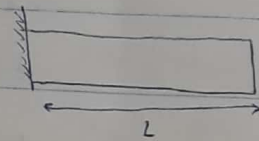
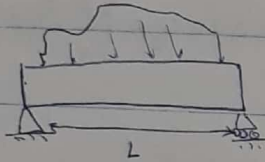


$$\frac{1}{f} = \frac{M(x)}{EI}$$

$$\frac{1}{f} = \frac{\frac{d^2 y}{dx^2}}{\left[1 + \left(\frac{dy}{dx}\right)^2\right]^{\frac{3}{2}}} \approx \frac{d^2 y}{dx^2} \rightarrow \boxed{\frac{d^2 y}{dx^2} = \frac{M(x)}{EI}}$$

$$\theta(x) = \frac{dy}{dx} = \int \frac{M(x)}{EI} dx + C_1$$

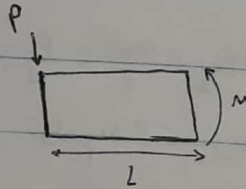
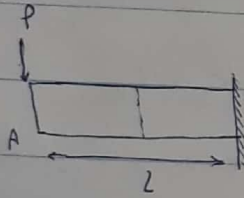
$$y(x) = \int dx \int \frac{M(x)}{EI} dx + C_1 x + C_2$$



$$y(x=0) = 0$$

$$y(x=L) = 0$$

$$y(x=0) = 0 \quad \theta(x=L) = 0$$



$$\frac{d^2 y}{dx^2} = \frac{-Px}{EI} \rightarrow \theta(x) = \frac{dy}{dx} = \int \frac{-Px}{EI} + C_1 = \frac{-Px^2}{2EI} + C_1$$

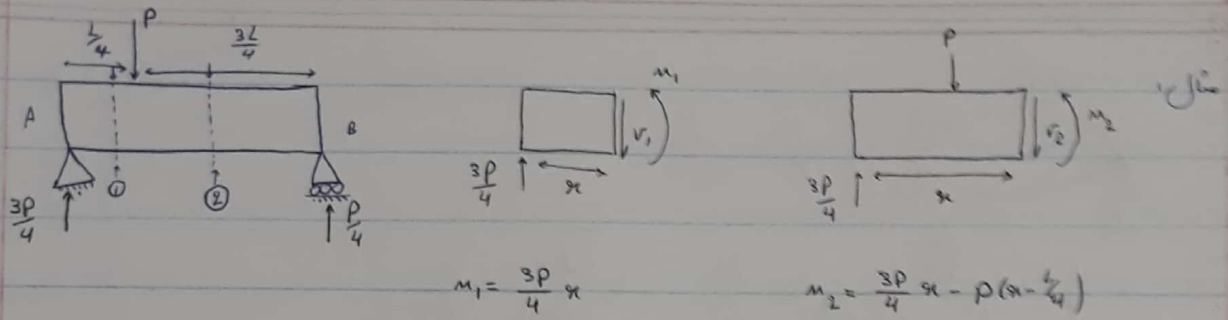
$$y = \int \frac{-Px^2}{2EI} + C_1 x + C_2 = \frac{-Px^3}{6EI} + C_1 x + C_2$$

$$\theta(x=L) = 0 \rightarrow \frac{-PL^2}{2EI} + C_1 = 0 \rightarrow C_1 = \frac{PL^2}{2EI}$$

$$y(x=L) = 0 \rightarrow \frac{-PL^3}{6EI} + \frac{PL^2}{2EI} \times L + C_2 = 0 \rightarrow C_2 = \frac{-PL^3}{3EI}$$

$$y(x) = \frac{-Px^3}{6EI} + \frac{PL^2}{2EI} x - \frac{PL^3}{3EI}$$

$$\theta_A = \theta(x=0) = \frac{-Px^2}{2EI} + \frac{PL^2}{2EI} \Big|_{x=0} = \frac{PL^2}{2EI}, \quad y_A = y(x=0) = \frac{-PL^3}{3EI}$$



$$\frac{d^2 y}{dx^2} = \frac{M(x)}{EI} \rightarrow EI \frac{d^2 y_1}{dx^2} = m_1 = \frac{3P}{4} x \rightarrow \begin{cases} EI \frac{dy_1}{dx} = \int \frac{3P}{4} x dx + C_1 = \frac{3Px^2}{8} + C_1 \\ EI y_1 = \int \frac{3P}{8} x^2 dx + C_1 x + C_2 = \frac{3P}{24} x^3 + C_1 x + C_2 \end{cases}$$

$$EI \frac{d^2 y_2}{dx^2} = m_2 = \frac{3P}{4} x - P(x - \frac{L}{4}) \rightarrow \begin{cases} EI \frac{dy_2}{dx} = \frac{3P}{8} x^2 - \frac{P}{2} (x - \frac{L}{4})^2 + C_3 \\ EI y_2 = \frac{Px^3}{8} - \frac{P}{6} (x - \frac{L}{4})^3 + C_3 x + C_4 \end{cases}$$

می بینیم که چهار معادله چهار مجهول خواهیم داشت پس بهتر است که از این روش استفاده نکنیم از روش عمق جیب استفاده کنیم (روش پوانتر نکسته).
 روش پوانتر نکسته:

$$\frac{d^2 y}{dx^2} = \frac{M(x)}{EI} \rightarrow m(x) = \frac{d^2 y}{dx^2} EI = \frac{3P}{4} (x) - P(x - \frac{L}{4})$$

$$\rightarrow \frac{dy}{dx} EI = \frac{3P}{8} \langle x \rangle^2 - \frac{P}{2} \langle x - \frac{L}{4} \rangle^2 + C_1 \rightarrow y EI = \frac{P}{8} \langle x \rangle^3 - \frac{P}{6} \langle x - \frac{L}{4} \rangle^3 + C_1 x + C_2$$

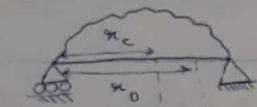
$$y_{(x=0)} = 0 \rightarrow C_2 = 0, \quad y_{(x=L)} = 0 \rightarrow \frac{P}{8} L^3 - \frac{P}{6} (\frac{3L}{4})^3 + C_1 L = 0 \rightarrow C_1 = \frac{7PL^2}{128}$$

همین روشی که همان تیر به کمک توزیع بار

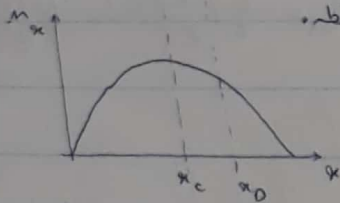
$$\frac{d^2 y}{dx^2} = \frac{M(x)}{EI}, \quad \frac{dM(x)}{dx} = V(x), \quad \frac{dV(x)}{dx} = -w(x)$$

$$\frac{d^3 y}{dx^3} = \frac{1}{EI} \frac{dM(x)}{dx} = \frac{V(x)}{EI}, \quad \frac{d^4 y}{dx^4} = \frac{1}{EI} \frac{dV(x)}{dx} = \frac{-w(x)}{EI} \rightarrow \frac{d^4 y}{dx^4} = \frac{-w(x)}{EI}$$

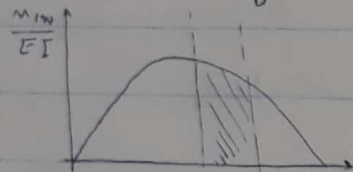
تغییر مکان تیر به روش گشتاور سطح



گشتاور سطح: اختلاف زاویه پدید می آید بین دو نقطه C و D از تیر برابر است با سطح زیر منحنی $\frac{M}{EI}$ بین دو نقطه.

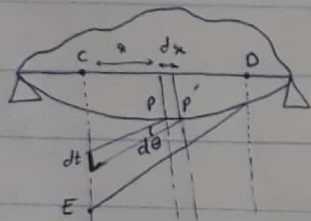


$$\frac{d^2 y}{dx^2} = \frac{M(x)}{EI} \quad \frac{dy}{dx} = \theta_{cm}$$

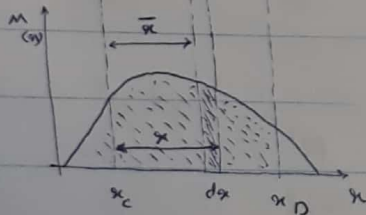


$$\frac{d\theta}{dx} = \frac{M(x)}{EI} \quad d\theta = \frac{M(x)}{EI} dx$$

$$\int_{\theta_c}^{\theta_D} d\theta = \int_{x_c}^{x_D} \frac{M(x)}{EI} dx = \theta_D - \theta_c = \theta_{D/C}$$



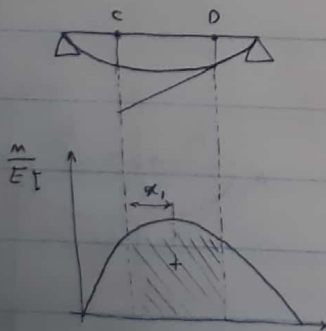
$$dt = x \cdot d\theta$$



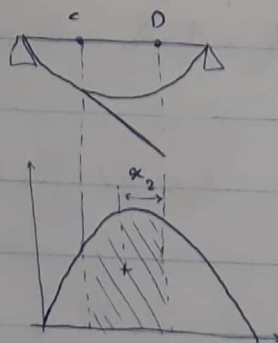
$$dt = x \frac{M(x)}{EI} dx$$

$$t_{D/C} = \int_{x_c}^{x_D} x \frac{M(x)}{EI} dx$$

تقریب دوم گشتاور سطح: فاصله عمود بر نقطه C از محاس بر نقطه D در تیر رو به برابر است با گشتاور اول سطح بین نقطه C و D نسبت به فاصله x_1 یا x_2



$$t_{D/C} = (\text{مساحت بین } x_D \text{ و } x_C) \times x_1$$



$$t_{D/C} = (\text{مساحت بین } x_D \text{ و } x_C) \times x_2$$

$\theta_B = 0, y_B = 0$

$\theta_{CD} = 1$

$\theta_{B/A} = \theta_B - \theta_A = A_{AB}, \quad A_{AB} = -\frac{1}{2} \left(\frac{PL}{EI} \right) \cdot L = -\frac{1}{2} \frac{PL^2}{EI}$

$\theta_B = \frac{-PL^2}{2EI}$

$y_B = t_{B/A} = \int \frac{M}{EI} dx$ (مساحت زیر منحنی θ_B از A تا B)

$t_{B/A} = A_{AB} \times \left(\frac{2}{3} L \right), \quad A_{AB} = \frac{-PL^2}{2EI} \rightarrow y_B = t_{B/A} = \frac{-PL^3}{3EI}$

$y_c = ? \quad \theta_A = ?$

$t_{A/C} = A_{Ac} \times \left(\frac{2}{3} \times \frac{L}{2} \right)$

$A_{Ac} = \frac{1}{2} \left(\frac{PL}{4EI} \right) \times \left(\frac{L}{2} \right) = \frac{PL^2}{16EI}$

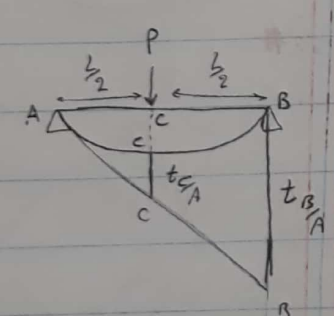
$y_c = t_{A/C} = \frac{PL^2}{16EI} \times \frac{2}{3} = \frac{PL^3}{48EI}$

$\theta_{AC} = \theta_A - \theta_C = \theta_A = A_{AB} = \frac{PL^2}{16EI}$

پوند

$t_{B/A} = A_{AB} \times \left(\frac{L}{2} \right), \quad A_{AB} = \frac{1}{2} \left(\frac{PL}{4EI} \right) (L) = \frac{PL^2}{8EI}$

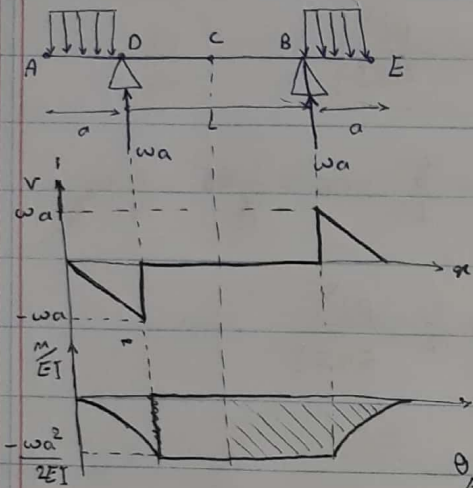
$t_{B/A} = \frac{PL^3}{16EI}$



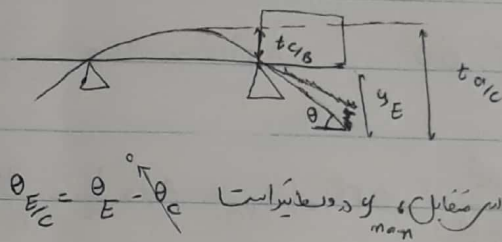
$ABB' \sim ACC' \rightarrow \frac{CC'}{BB'} = \frac{AC}{AB} = \frac{L/2}{L} \rightarrow CC' = \frac{1}{2} BB' = \frac{1}{2} t_{B/A} = \frac{PL^3}{32EI}$

$$y_c = CC'' - t_{CA} \quad t_{CA} = A_{AC} \times \frac{L}{6} \quad A_{AC} = \frac{PL^2}{16EI}$$

$$t_{CA} = \frac{PL^3}{96EI} \rightarrow y_c = CC'' - t_{CA} = \frac{PL^3}{48EI}$$



$$\theta_E = ? \quad y_E = ?$$



جهت پایه در مقابل و در دست راست مان

$$\theta_E = \theta_{E/C} = A_{EC} = A_1 + A_2 = \frac{-wa^2L}{4EI} - \frac{wa^3}{6EI} = \frac{-wa^2}{12EI} (3L+2a)$$

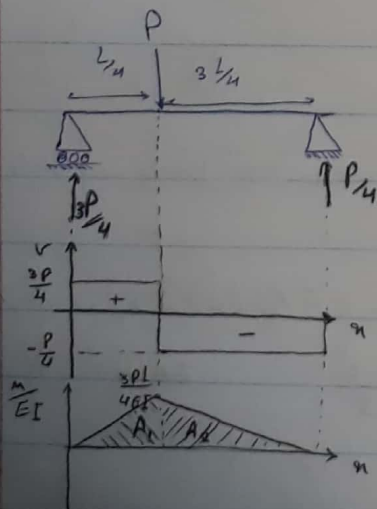
$$A_1 = \frac{-wa^2}{2EI} \times \frac{L}{2} = \frac{-wa^2L}{4EI}$$

$$A_2 = \frac{1}{3} \left(\frac{wa^2}{2EI} \right) (a) = \frac{wa^3}{6EI}$$

$$y_E = t_{E/C} - t_{D/C}$$

$$t_{E/C} = A_1 \times \left(\frac{L}{4} + a \right) + A_2 \times \left(\frac{3a}{4} \right) = -\frac{wa^3L}{4EI} - \frac{wa^2L^2}{16EI} - \frac{wa^4}{8EI}$$

$$t_{D/C} = A_1 \times \frac{L}{4} \rightarrow y_c = \frac{-wa^3}{8EI} (3L+a)$$



$$\theta_{D/A} = \theta_D - \theta_A$$

$$t_{D/A} = A_1 \left(\frac{L}{12} + \frac{3L}{4} \right) + A_2 \left(\frac{2}{3} \times \frac{3L}{4} \right)$$

$$A_1 = \frac{1}{2} \left(\frac{3PL}{16EI} \right) \left(\frac{L}{4} \right) = \frac{3PL^2}{128EI}$$

$$A_2 = \frac{1}{2} \left(\frac{3PL}{16EI} \right) \left(\frac{3L}{4} \right) = \frac{9PL^2}{128EI}$$

$$t_{B/A} = \frac{7PL^3}{128EI}$$

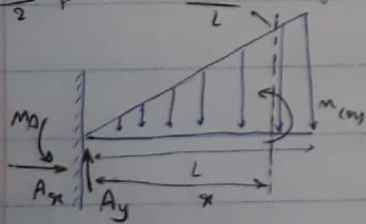
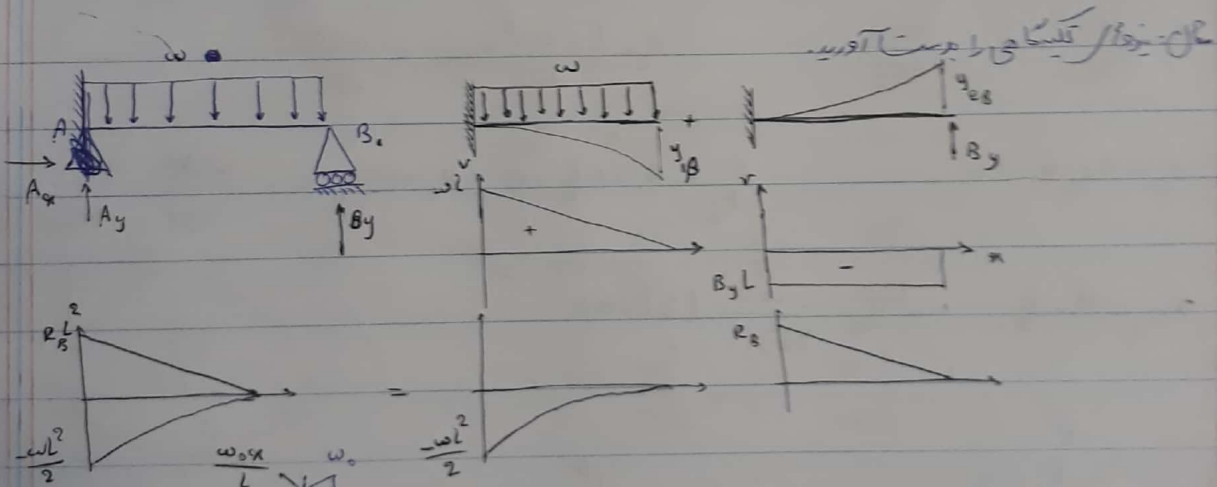
$$\tan \theta_A = \theta_A = \frac{t_{B/A}}{L} \rightarrow \theta_A = \frac{7PL^3}{128EI}$$

$$\theta_{D/A} = \theta_D - \theta_A \quad A_1 = \theta_D - \frac{7PL^3}{128EI} \rightarrow \theta_D = \frac{-PL^3}{32EI}$$

$$y_D = DD'' - \theta_D L \quad A \Delta DD'' \sim ABB' \rightarrow \frac{DD''}{BB'} = \frac{L}{4} \rightarrow DD'' = \frac{1}{4} BB' = \frac{1}{4} t_{B/A}$$

$$= \frac{1}{4} \times \frac{7PL^3}{128EI} = DD'' = t_{D/A} = A_1 \times \frac{L}{12} = \frac{3PL^3}{128EI} \times \frac{L}{12} = \frac{PL^3}{512EI}$$

$$\rightarrow y_D = DD'' - t_{D/A} = \frac{-3PL^3}{256EI}$$



$$\sum F_y = 0 \rightarrow Ay - \frac{w \cdot L}{2} = 0 \rightarrow Ay = \frac{w \cdot L}{2} \quad \sum F_x = 0 \rightarrow Ax = 0$$

$$\sum M_A = 0 \rightarrow M_A - \frac{w \cdot L}{2} \left(\frac{2L}{3} \right) = 0 \rightarrow M_A = \frac{w \cdot L^2}{3}$$

$$EI \frac{d^2y}{dx^2} = M(x)$$

$$M_{(m)} + M_A - Ayx + \frac{\omega x^2}{2L} \left(\frac{x}{3}\right) = 0 \rightarrow M_{(m)} = Ayx - M_A - \frac{\omega x^3}{6L}$$

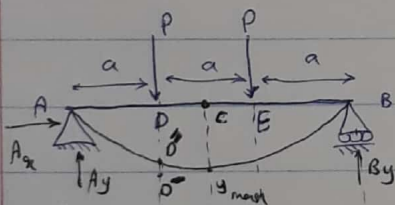
$$\rightarrow EI \frac{d^2y}{dx^2} = M_{(m)} = Ayx - M_A - \frac{\omega x^3}{6L} = \frac{\omega L}{2} x - \frac{\omega L^3}{3} - \frac{\omega x^3}{6L}$$

$$\rightarrow EI \frac{dy}{dx} = \frac{\omega L}{4} x^2 - \frac{\omega L^3}{3} x - \frac{\omega x^4}{24L} + C_1$$

$$\rightarrow EI y = \frac{\omega L}{12} x^3 - \frac{\omega L^3}{6} x^2 - \frac{\omega x^5}{120L} + C_1 x + C_2$$

$$x=0 \rightarrow y=0 \Rightarrow C_2=0, \quad x=L \rightarrow \theta=0 \Rightarrow C_1=0$$

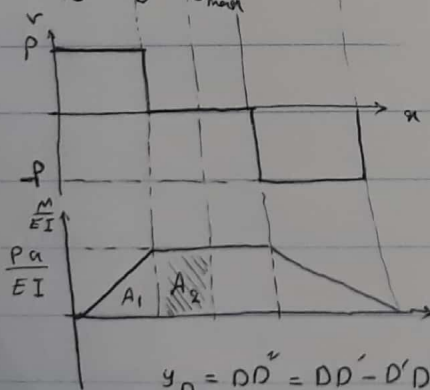
$$y_{(m)} = \frac{\omega L x^3}{12} - \frac{\omega L^3 x^2}{6} - \frac{\omega x^5}{120L}$$



مثال: بارهای گویا و گویا y_D, θ_D

$$\rightarrow A_x=0, A_y=P, B_y=P$$

بعلت تعادل بارها:



$$\theta_D = \theta_{D/c} + \theta_c = A_2$$

$$A_2 = \left(\frac{a}{2}\right) \left(\frac{Pa}{EI}\right) = \frac{Pa^2}{2EI} = \theta_D$$

$$y_D = DD'' = DD' - D'D'' \rightarrow DD'' = y_{max} = t_{A/c} = A_1 \left(\frac{3}{2}a\right) + A_2 \left(\frac{5a}{4}\right)$$

$$\rightarrow D'D'' = t_{D/c} = A_2 \left(\frac{a}{4}\right) = \frac{Pa^2}{2EI} \left(\frac{a}{4}\right)$$

$$\rightarrow DD'' = DD' - t_{D/c} = \frac{5}{8} \left(\frac{Pa^3}{EI}\right)$$